95

magnets in use all the time—that is, in continuous duty—the watts per square inch should not be more than .7.

For magnets in use only a few minutes at a time—that is, intermittent duty—our value can be 2.8 or less.

For magnets for very short time of work—that is, momentary duty—the value can be as high as 11.2.

The rule to find this value is: first find the value AT ÷ winding space and this answer multiplied by itself. Let us call this

$$\left(\frac{\text{AT}}{\text{W.S.}}\right)^2$$

Then our complete rule is: Watts per square inch surface =

 $\frac{\text{(MS.)}^2 \times .78 \times \text{M.L.T.}}{\text{Depth} \times \text{Space factor}} \times \text{M.L.T.} + 3.1416 \times \text{depth} \times 1,000,000$

This means: $\left(\frac{AT}{W.S.}\right)^2$ multiplied by .78, this result by the mean length of turn. This we will call Answer No. 1. Also, multiply the winding depth by the space factor, this result by the sum of the mean length of turn and 3.1416 times the winding depth, and this result by 1,000,000. This we will call Answer No. 2.

Space Factor. In this formula you find the space factor. This is a value which represents the decimal part of the winding space actually occupied by the bare copper. For example, if in Table B, we see that 2630 turns of enamel wire, size No. 25, can be wound in one square inch, but 2630 turns of bare, No. 25, have a cross section of only

.000254 2630 7620 1524 508 .668020

Cross section in inches = circular mils \times .785 \times .000001. A mil = .001 inches and a square mil = .00001 of a square inch, that is, .668 of a square inch, then .668 \div 1 = .668 or the ratio of the bare copper in the winding space to the winding space.

Table B values are for coils wound evenly row on row. It is very seldom that coils are wound as carefully as this so it is usual to use a space factor lower than what is shown in the table. A good plan will be to subtract .1 from the value found for all irregular wound coils.

Now we can attempt to work our problem. Let us call our space factor .57.

$$Watts = \frac{\left(\frac{2.94}{1.5}\right)^2 \times .78 \times 3.157}{.375 \times .57 \times 4.345 \times 1,000,000}$$

$$1.5) \frac{294}{15} \left(196\right)$$

$$1.5) \frac{144}{135}$$

$$196$$

$$11764$$

$$196$$

$$11764$$

$$196$$

$$196$$

$$38416$$

$$38416$$

$$307328$$

$$268912$$

$$29964.48$$
(C)

call it 930000	.92874375	106875 85500 64125	21375 4.345	.57 2625 1875	.375	29964.48 3.157 20975136 14982240 2996448 8989344 94597.86336 Answer No. 1.
Answer No. 2.						
<u>(2</u>	F		(E)			()

Dividing Answer No. 1 by No. 2 we have

number of turns of wire per coil. This shows we have a safe beating, and we can now determine the

RULES FOR TURNS PER COIL

tion in square inches; you will have the turns required. space factor. Divide this answer by the area of the wire cross sec-Multiply width of winding by the depth and the result by the

> Turns = width X depth X space factor Area of wire section

inches, the activity .57, and the area of our wire = .000254 inches Example. Our winding space is 1.5 inches, the depth .375

Turns =
$$\frac{1.5 \times .375 \times .57}{.000254}$$
 =

1.5 ,375 75 105 45 .5625 .57 39375 28125

1582 1524 508 77 .320625 (1262 + call it 1263

wire, size No. 25. Then we will wind our coils with 1263 turns of enameled copper

3.1416 inches, our total number of turns have a length of B -7Let us prove our figures to be sure of them. If our M.L.T. is

12) 3967.8408 inches (330.65 ft. call it 331.

36 36 078

The resistance per ft., see Table A = .03231.

10.69461 ohms. call it 10.7 ohms.

We are to connect two coils together in series so our total resistance = 21.4 ohms. We must multiply this resistance by 1.15 to allow for the fact that after heating a well designed copper coil will increase its resistance at about this value

21.4 1.15 1070 214 214

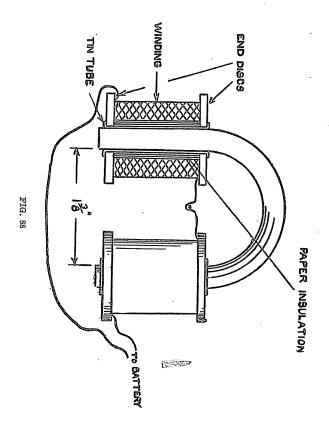
24.610 ohms hot.

Amperes flowing $=\frac{6 \text{ volts}}{24.6} = .244 \text{ amperes}$

1263 turns
.244 amperes
5052
5052
2526
308 .172 ampere turns

Our required number is 294, so we show a difference in our favor of 14 ampere turns.

Now we can put our coils on the magnet yoke. Fasten them in place by wrapping some sticking-tape around the steel just on each side of the fibre washer. Let the ends of the wire be brought out at least a foot from the coil so you can make the necessary connections.



many times to design magnets enough for all practical purposes and these rules have been used insulation and the other details of construction. This is close Figure 88 shows one of these coils split in half to show the paper

MOVING CORE MAGNETS

chapter on magnetic toys and tricks is one of these. In the circuit suck their core up into them. from that of a lifting magnet. breaker, also, the pull exerted on the moving core, is quite different Moving core or plunger magnets are of the type which pull or The magnetic guns described in the

only about one-half of the full value at the ends. netic centers of the coil and core are in the same place. causes the soft iron core, or plunger as it is often called, to become and also some very short ones. passed the middle point of the coil, except for some very long coils you will see that the greatest pull comes just after the plunger has than the solenoid winding, the pulling effect stops when the magmagnetized and sucked into the hole in the solenoid. As the plunger by induction until it becomes saturated. If it is not much longer passes along, it becomes more and more filled with magnetic lines The magnetizing force of a solenoid is greatest at its center and From this That fact

such a magnet cated than are those for the lifting magnet, so we will not give them here, but a few points may be mentioned which will help in planning The rules for these plunger magnets are somewhat more compli-

if possible. The length of the pull is in proportion to the coil length. Make your core at least one and one-half times the length Make your coil with a diameter about three times its diameter

opposite to that which the plunger is to enter-To increase the pull, a short fixed core can be placed in the end

POLARIZED MAGNETS

direction of current flowing in the coils. permanent magnet in place of the usual soft iron and is placed current in the coil is reversed. the direction in which it is moved can be changed by changing the between the poles of the electro-magnet instead of in front of them An electro-magnet pulls its armature one way even though the But if the armature is made of a

EXPLANATIONS FOR TABLE

A mil = 1/1000 or our memory
A circular mil = diameter of the wire in mils × itself. S.C.C. = Single cotton cover. A mil = 1/1000 of an inch. D.C.C. = Double cotton cover. Enam. = Enameled.

33333		26 27 27 30	22 22 23 25 4	15 15 20 20	112 0. 113	00000	44840	B&S	=
.0050	008928 007950 007080 006305 005615	.01594 .0142 .01264 .01264 .01126 .01003	.02846 .02535 .0257 .02257 .02010 .01790	.05082 .04526 .0403 .03589 .03196	0.09074 .08081 .07196 .0648 .05707	.1620 .1443 .1285 .1144 .1019	. 2893 . 2576 . 2294 . 2043 . 1819	Bare	
.0055 .0049 .0044	.0097 .0087 .0077 .0069 .0062	.0171 .0153 .0136 .0122 .0109	.0302 .0269 .0241 .0215 .0192	.0528 .0470 .0421 .0377 .0337	.0927 .0828 .0704 .0661 .0591	.1306 .1165 .1040		Enam.	
.00900	.0129 .01195 .01108 .01030 .00961	.0199 .0182 .0166 .0153 .0140	.0335 .0293 .0261 .0241 .0219	.0558 .0503 .0453 .0400 .0370	.0967 .0868 .078 .0701 .0631	.169 .151 .1355 .1355 .1214 .1079	.189	S.C.C	
.01300 .01245 .01196	.0169 .01595 .01508 .01430 .01361	.0239 .0222 .0206 .0193 .0180	.0385 .0333 .0306 .0281 .0259	.0608 .0553 .0503 .0459 .0420	.1017 .0918 .083 .0751 .0681	0.174 0.156 0.1416 0.1274 0.1129	0.303 0.272 0.242 0.242 0.216 0.194	D.C.C.	
.00700	.0109 .00995 .00908 .00830 .00/761	.0179 .0162 .0146 .0133 .0120	.0305 .0273 .0246 .0221 .0199	.0528 .0473 .0423 .0379 .0340			,	DIAMETER Single Silk	Table
.00880 .00825 .00776	.0127 .01175 .01088 .0101 .0101	.0197 .0180 .0164 .0151 .0138	.0323 .0291 .0264 .0239 .0217	.0546 .0491 .0441 .0397 .0358		,		Double Silk	A
25.0 19.83 15.72	79.70 63.21 50.13 39.75 31.52	254.1 201.5 159.8 126.7 100.5	810.1 642.4 509.5 404.0 320.4	2583 2048 1624 1288 1022	8234 6530 5178 4107 3257	26250 20820 16510 13090 10380	83690 66370 52630 41740 33100	Circular Mils	
13210 16660 21010	4145 5227 6591 8311 10480	1300 1639 2067 2607 3287	407.8 514.2 648.4 817.6	127.9 161.3 203.4 256.5 323.4	40.12 50.59 63.79 80.44 101.4	12.58 15.87 20.01 25.23 31.82	3.947 4.977 6.276 7.914 9.98	Foot per lb.	
.4142 .5222 .6585	.1299 .1638 .2066 .2605 .3284	.04075 .05138 .06479 .08170 .1030	.01278 .01612 .02032 .02563 .03231	.004009 .005055 .006374 .008038 .01014	.001257 0.0001586 .001999 0.002521 0.003179	0.0003944 0.0004973 0.0006271 0.0007908 0.0009972	70.0001237 70.000156 70.0001967 60.000248 0.0003128	Ohms per ft.	

TURNS	
PER	Ӹ
SQUARE	ble B
INCH	

. 38 39 40	33 34 35 36 37	28 29 30 31 32	23 24 25 25 26 27	18 19 20 21 21 22	13 14 15 16	8 9 10 11 12	в & s	
49100 62600 77600	16200 19950 25000 31700 39600	5250 6510 8175 10200 12650	1665 2100 2630 3320 4145	548 681 852 1065 1340	177 221 277 277 348 437	57 72 90 113 141	Beld- Enamel	- AMARIAN SANAS
14900 16600 18400	7780 9010 10300 11750 13250	3500 4120 4900 5770 6700	1370 1665 2020 2445 2925	472 581 712 868 1128	160 198 245 312 383	53 66 84 104 129	Single Cotton	
6510 6935 7450	4140 4595 5070 5550 6045	2250 2560 2930 3330 3720	1030 1215 1420 1690 1945	378 455 545 650 865	140 · 171 208 260 316	48 59 76 93 114	Double Cotton	
27300 31700 36700	11850 14250 16800 19850 23300	4600 5530 6810 8260 9870	1620 2010 2470 3005 3680	548 682 848 1055 1315	351 437		Single Silk	
15960 17850 19900	8160 9480 10870 12430 14100	3620 4270 5100 6010 6990	1400 1705 2070 2510 3010	503 619 761 935 1150	327 405		Double Silk	

GILBERT MAGNETIC FUN AND FACTS

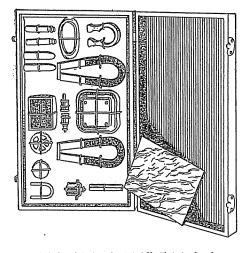
Table C AMPERE TURNS AND MAGNETIC DENSITY

D'VCI	Tuon	7.1		,	,				
CASL	CAST TROM	CAST STEEL	TEEL	COLD KOLLED STEEL	ED STEEL	ANNEALED SHT.	T. IRON		
Mag. Density B	Amp. Turns per In.								
20000	. 23	20000	7	20000	6	20000	3		
25000	31	25000	7	25000	9.	25000	ယ	<u>200</u> 0.10.20.	
30000	44	30000	∞	30000	7	30000	ယ		
35000	61	35000	9	35000	8	35000	4	•	
40000	87	40000	9.5	40000	∞	40000	4		
45000	Cast	45000	10	45000	8.5	45000	4		
50000	Highly Sath-	50000	<u>⊢</u>	50000	10	50000	Ċτ	أو 2 كيان بالمسام ميت	
55000	rated	55000	13	55000		55000	6		
.60000	Density	60000	15.5	60000	13	60000	∞		
65000	40000	65000	17.5	65000	15	65000	10		
70000		70000	21	70000	17	70000	13	-	
75000		75000	25.5	75000	21	75000	16	., ~ 6,	
80000		80000	31	80000	25	80000	20	<u>-</u> 980 2 1 3 4	
85000		<u>§</u> 5000	38	85000	30	85000	25	ت البحق	
90000	`	90000	50	90000	38	90000	33	an like Gran de a	
95000		95000	70	95000	47	95000	42		
100000		100000	110	100000	61	100000	59		

DECIMAL	
EQUIVALENTS	Table D
9	
ONE	
INCI	

3/64	1/2	31/64	15/32	29/64	7/16	27/64	13/32	25/64	3/8	11/32	21/64	5/16	19/64	9/32	17/64	$1/4 \dots$	15/64	7/32	13/64	3/16	11/64	5/32	9/64	1/8	7/64	3/32	5/64	1/16	3/64	1/32	T/07
							:	:		:	:	:	:		:		:	:	:	:		:	:	:	:		:	:	:	:	:
٠	٠	٠	•	•		•	٠			•		•		٠	٠																
•	•	•	•	٠	•	٠	•	٠	٠	•	•	•	•	٠	٠	٠	٠			٠	•	•	•	٠	•	•	•		•		•
.515625	.v.	.484375	.46875	.453125	.4375	.421875	.40625	.390625	.375	.34375	.328125	.3125	.296875	.28125	.265625	.25	.234375	.21875	.203125	.1875	.171875	.15625	.140625	.125	.109375	.09375	.078125	.0625	.046875	.03125	· OTOCAC
		63/64	31/32	61/64	15/16	59/64	29/32	57/64	7/8	55/64 .	27/32 .	53/64 .	13/16 .	51/64 .	25/32 .	49/64 .	3/4 .	47/64 .	23/32 .	45/64 .	11/16 .	43/64 .	21/32 .	41/64 .	5/8 .	39/64	19/32 .	37/64 .	9/16 .	35/64 .	11/02 .
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	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	٠	•	٠	•	•	•	•	•	•	•	•	٠	•	•	•	•
	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	•	٠	٠	•	•	•	•	•	•	٠	•	•	٠	•	•	٠
		•	•	•	•	•	•	•	•	•	•	•	•	:	•	•	•	•	•	•	•	•	•	•	•	•	٠	•	•	•	•
	•	.984375	.96875	.953125	.9375	.92187	.90625	.89062	.875	.85937	.84375	.82812	. 8125	.79687	.78125	.76562	. 75	.73437.	.71875	. 70312	.6875	.67187	.65625	.64062	. 625	.60937	.5937	.57812	.5625	.54687	. DOLLO

4 1/4 4 3/8		~1,	3 3/4	س ب	رس	<u> 1</u>	_	:		ųυ	-	بري	2 1/4				ω	ωį	<u> </u>	N.	1 1/8	_	15/16	7	13/16		11/16	8/2 01/6	1/2		3/8		3/10	. ~	_	1/32	1/64	Diam.	CIR	
13.3518			11.7810			10.2102				9 6304				6.6759	-						3 9270										1.1781	.9817	7854	.3927	. 1963	.0982	.0491	Circum.	CIRCUMFERENCE	
14. 1863 15. 0330	12.5004		11.0447			8.2958	7.6699	7 0686	6 4018	5.4119	4,908/	4.4301	3.9761	3.5466	3.1416	2.7612	2.4053	2.0739	1.7671	1 4849	1 2272	./854	. 6903	.6013	.5185	.4418	3712	2068	. 1963	.1503	.1104	0767	0401	.0123	.0031	.0008	.0002	Area in Sq. Ins.	INCES AND	Table
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31.0233 31.4160	30.6306		29.4525				27.4890	27.0963	26.7036	26 3109	25 0182	27.13.50	24.7401	24.34/4	23.9547	23.5620	23, 1693	22.7766			21.5985						18.8496			17.2788	-		16 1007	15 7080		14.5299		Circum.	9	
76.589 78.540	`~:				ıω																37.1224		33.1831			29.4648	28.2744	27 1086	24.8505	23.7583	22.6907	21.6476	20 6290	10.0333	10 6555	16.8002	15.9043	Area in Sq. Ins.	CIRCLES	



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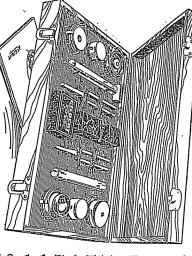
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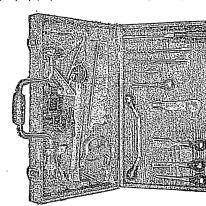
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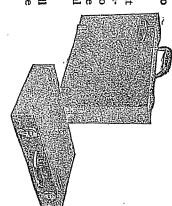
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